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Multi-region relaxed magnetohydrodynamics with anisotropy and flow

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We present an extension of the multi-region relaxed magnetohydrodynamics (MRxMHD) equilibrium model that includes pressure anisotropy and general plasma flows. This anisotropic extension to our previous isotropic model is motivated by Sun and Finn's model of relaxed anisotropic magnetohydrodynamic equilibria. We prove that as the number of plasma regions becomes infinite, our anisotropic extension of MRxMHD reduces to anisotropic ideal MHD with flow. The continuously nested flux surface limit of our MRxMHD model is the first variational principle for anisotropic plasma equilibria with general flow fields. © 2014 AIP Publishing LLC.

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I. INTRODUCTION

The construction of magnetohydrodynamic (MHD) equilibria in three-dimensional (3D) configurations is of fundamental importance for understanding toroidal magnetically confined plasmas. The theory and numerical construction of 3D equilibria is complicated by the fact that toroidal magnetic fields without a continuous symmetry are generally a fractal mix of islands, chaotic field lines, and magnetic flux surfaces. Hole *et al.*² have proposed a variational method for isotropic 3D MHD equilibria that embrace this structure by abandoning the assumption of continuously nested flux surfaces usually made when applying ideal MHD. Instead, a finite number of flux surfaces are assumed to exist in a partially relaxed plasma system. This model, termed a multi-region relaxed MHD (MRxMHD) model, is based on a generalization of the Taylor relaxation model^{3,4} in which the total energy (field plus plasma) is minimized subject to a finite number of magnetic flux, helicity, and thermodynamic constraints.

Obtaining 3D MHD equilibria that include islands and chaotic fields is a difficult problem, and a number of alternative approaches have been developed, including iterative approaches^{5,6} and variational methods for linearized perturbations about equilibria with nested flux surfaces.^{7,8} In general, variational methods have more robust convergence guarantees than iterative methods, and all else being equal, are usually preferable. However, variational methods for plasma equilibria require constraints to be specified and enforced in order to obtain non-vacuum solutions. The variational methods employed by Hirshman *et al.*⁷ and Helander and Newton⁸ specify these constraints in terms of the flux surfaces of a nearby equilibrium with nested flux surfaces. These methods are therefore necessarily perturbative, as opposed to the iterative methods of Reiman and Greenside⁵ and Suzuki *et al.*⁶ which aim to solve the full nonlinear 3D MHD equilibrium problem. The MRxMHD model is a variational method and must also enforce constraints to obtain non-vacuum solutions. The approach taken by MRxMHD

is to assume the existence of a finite number of good flux surfaces, and to enforce plasma constraints in the regions bounded by these good flux surfaces. This approach allows MRxMHD to solve the full nonlinear 3D MHD equilibrium problem with the assumption that there exist a finite number of flux surfaces that survive the relaxation process. This assumption is motivated by the work of Bruno and Laurence,⁹ who have proved that for sufficiently small deviations from axisymmetry such flux surfaces will exist and that they can support non-zero pressure jumps.

The MRxMHD model has seen some recent success in describing the 3D quasi-single-helicity states in RFX-mod;¹⁰ however, it must be extended to include anisotropic pressure as significant anisotropy is observed in high-performance devices, particularly in the presence of neutral beam injection and ion-cyclotron resonance heating.^{11–13} Our extension of MRxMHD to include pressure anisotropy is guided by the work of Sun and Finn¹ who studied a model for relaxed anisotropic plasmas by constraining the parallel and perpendicular entropies $S_{\parallel} = \int \rho \ln(p_{\parallel} B^2 / \rho^3) d^3\tau$ and $S_{\perp} = \int \rho \ln[p_{\perp} / (\rho B)] d^3\tau$, in addition to the flux and magnetic helicity constraints considered by Taylor.⁴ The model studied by Sun and Finn is a special case of the single plasma-region, zero-flow limit of the anisotropic MRxMHD model presented in this paper.

In the opposite limit, as the number of plasma interfaces becomes large and the plasma contains continuously nested flux surfaces, it is desirable for anisotropic MRxMHD to reduce to anisotropic ideal MHD. We prove this limit to be true in Sec. III, demonstrating that anisotropic MRxMHD (with flow) essentially “interpolates” between an anisotropic Taylor-Woltjer relaxation theory on the one hand and anisotropic ideal MHD with flow on the other. The continuously nested flux surface limit of anisotropic MRxMHD is, to the authors' knowledge, the first variational energy principle for anisotropic plasma equilibria with general flow fields. This is a generalization of earlier work developing variational principles for isotropic plasma equilibria with flow.¹⁴

This paper is structured as follows: in Sec. II, we give a summary of the MRxMHD model and its solution for a finite

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number of plasma regions before presenting our extension to include pressure anisotropy. In Sec. III, we prove that this extension of MRxMHD reduces to anisotropic MRxMHD with flow in the limit of continuously nested flux surfaces. This is followed by an example application of the anisotropic MRxMHD model to a reversed-field pinch (RFP) plasma in Sec. IV. The paper is concluded in Sec. V.

II. THE MULTI-REGION RELAXED MHD MODEL

A. The isotropic, zero-flow limit

The model we present in this paper is an extension of the MRxMHD model introduced previously.^{2,15–17} Briefly, the MRxMHD model consists of N nested plasma regions \mathcal{R}_i separated by ideal MHD barriers \mathcal{I}_i (see Fig. 1). Each plasma region is assumed to have undergone Taylor relaxation⁴ to a minimum energy state subject to conserved fluxes and magnetic helicity. The MRxMHD model minimizes the plasma energy

$$E = \sum_i E_i = \sum_i \int_{\mathcal{R}_i} \left(\frac{1}{2} \mathbf{B}^2 + \frac{1}{\gamma - 1} p \right) d^3\tau, \quad (1)$$

where we have used units such that $\mu_0 = 1$, and the minimization of Eq. (1) is subject to constraints on the plasma mass M_i and the magnetic helicity K_i , which are given by

$$M_i = \int_{\mathcal{R}_i} \rho d^3\tau, \quad (2)$$

$$K_i = \int_{\mathcal{R}_i} \mathbf{A} \cdot \mathbf{B} d^3\tau - \Delta\psi_{p,i} \oint_{\mathcal{C}_{p,i}^<} \mathbf{A} \cdot d\mathbf{l} - \Delta\psi_{t,i} \oint_{\mathcal{C}_{t,i}^>} \mathbf{A} \cdot d\mathbf{l}, \quad (3)$$

where p is the plasma pressure, ρ is the plasma mass density, \mathbf{A} is the magnetic vector potential, and the loop integrals in Eq. (3) are required for gauge invariance. The plasma in each volume is assumed to obey the adiabatic equation of

state $\sigma_i = p/\rho^\gamma$ with σ_i constant in each region. Additionally, each plasma region \mathcal{R}_i is bounded by magnetic flux surfaces and is constrained to have enclosed toroidal flux $\Delta\psi_{t,i}$ and poloidal flux $\Delta\psi_{p,i}$. The $\mathcal{C}_{p,i}^<$ and $\mathcal{C}_{t,i}^>$ are circuits about the inner (<) and outer (>) boundaries of \mathcal{R}_i in the poloidal and toroidal directions, respectively.

Minimum energy states of the MRxMHD model are stationary points of the energy functional

$$W = \sum_i \left[E_i - \nu_i (M_i - M_i^0) - \frac{1}{2} \mu_i (K_i - K_i^0) \right], \quad (4)$$

where ν_i and μ_i are Lagrange multipliers, respectively, enforcing the plasma mass and magnetic helicity constraints, and the M_i^0 and K_i^0 are, respectively, the constrained values of the plasma mass and magnetic helicity.

Setting the first variation of Eq. (4) to zero gives¹⁵

$$\nabla \times \mathbf{B} = \mu_i \mathbf{B}, \quad (5)$$

$$p_i = \text{const}, \quad (6)$$

$$0 = \left[\left[p_i + \frac{1}{2} \mathbf{B}^2 \right] \right], \quad (7)$$

where Eqs. (5) and (6) apply in each plasma region \mathcal{R}_i , Eq. (7) applies on each ideal interface \mathcal{I}_i , and $[[x]] = x_{i+1} - x_i$ denotes the change in the quantity x across the interface \mathcal{I}_i .

B. Including the effects of plasma flow

In previous work, we extended the MRxMHD model to include plasma flow.¹⁸ That model is defined by minimizing the plasma energy

$$E = \sum_i E_i = \sum_i \int_{\mathcal{R}_i} \left(\frac{1}{2} \rho \mathbf{u}^2 + \frac{1}{2} \mathbf{B}^2 + \frac{1}{\gamma - 1} p \right) d^3\tau, \quad (8)$$

where \mathbf{u} is the mean plasma velocity. The minimization of the plasma energy is subject to constraints on the plasma mass and helicity given by Eqs. (2) and (3), and additional constraints on the flow helicity C_i and toroidal angular momentum L_i , which are given by

$$C_i = \int_{\mathcal{R}_i} \mathbf{B} \cdot \mathbf{u} d^3\tau, \quad (9)$$

$$L_i = \hat{\mathbf{Z}} \cdot \int_{\mathcal{R}_i} \rho \mathbf{r} \times \mathbf{u} d^3\tau = \int_{\mathcal{R}_i} \rho R \mathbf{u} \cdot \hat{\phi} d^3\tau, \quad (10)$$

where the (R, Z, ϕ) cylindrical coordinate system is used with $\hat{\mathbf{Z}}$ a unit vector pointing along the axis of symmetry, and $\hat{\phi}$ the toroidal angle.

As described in detail in Dennis *et al.*,¹⁸ constraining the toroidal angular momentum L_i in each plasma region requires assuming the plasma to be axisymmetric. A more appropriate model for 3D MHD structures is obtained if instead only the total toroidal angular momentum $L = \sum_i L_i$ is constrained.¹⁹ This only requires the assumption that the

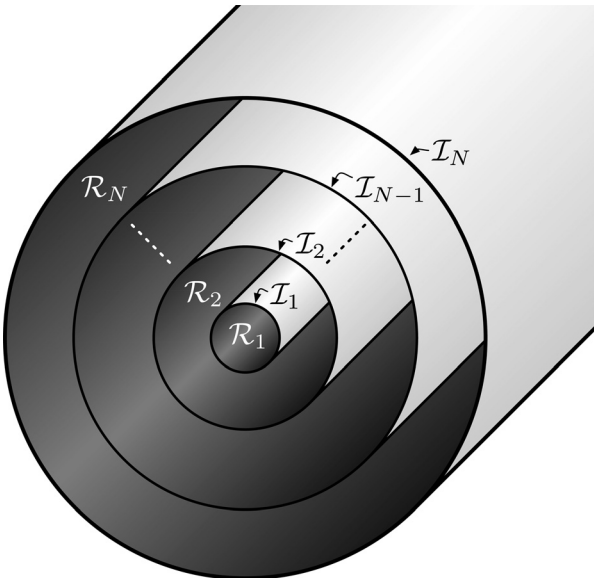


FIG. 1. Schematic of magnetic geometry showing ideal MHD barriers \mathcal{I}_i and the relaxed plasma regions \mathcal{R}_i .

outer plasma boundary be axisymmetric. In the case of stellarators or other situations where the plasma boundary is not axisymmetric, the toroidal angular momentum constraint must be relaxed entirely.

In our earlier work,¹⁸ we solved this variational problem assuming the adiabatic equation of state $p = \sigma_i \rho^\gamma$, where σ_i is constant in each plasma region. This is appropriate if relaxation is assumed to occur fast enough that heat transport is negligible. An alternative approach, which was taken by Finn and Antonsen,²⁰ is to instead maximize the plasma entropy in each region, while conserving the plasma energy, mass, helicity, flow helicity, and angular momentum. This is equivalent to assuming that parallel heat transport is rapid and that the plasma has reached thermal equilibrium along each field line. Finn and Antonsen²⁰ prove that the Euler-Lagrange equations (Eqs. (5)–(7)) obtained from this approach are identical to those obtained by instead minimizing the plasma energy while holding the plasma entropy and other constraints fixed. The only difference between these two approaches is that for a given initial state, the final relaxed states will be different if entropy is maximized while conserving energy versus minimizing energy while conserving entropy. In this article, we will take the approach of minimizing energy for consistency with our earlier work,^{2,15–18,21} however identical Euler-Lagrange equations are obtained with either approach.

The two equations of state used to complete the MRxMHD model with flow, namely, assuming the adiabatic equation of state $p = \sigma_i \rho^\gamma$ or conserving the plasma entropy are described in Secs. II B 1 and II B 2.

1. Adiabatic equation of state

If the adiabatic equation of state $p = \sigma_i \rho^\gamma$ is assumed, the minimum energy states are stationary points of the energy functional

$$W = \sum_i \left[E_i - \nu_i (M_i - M_i^0) - \frac{1}{2} \mu_i (K_i - K_i^0) - \lambda_i (C_i - C_i^0) - \Omega_i (L_i - L_i^0) \right], \quad (11)$$

where λ_i and Ω_i are Lagrange multipliers enforcing the flow-helicity and angular momentum constraints.

We have previously shown that the minimum energy states of this model satisfy¹⁸

$$\nabla \times \mathbf{B} = \mu_i \mathbf{B} + \lambda_i \nabla \times \mathbf{u}, \quad (12)$$

$$\rho \mathbf{u} = \lambda_i \mathbf{B} + \rho \Omega_i R \hat{\phi}, \quad (13)$$

$$\nu_i = \frac{1}{2} \mathbf{u}^2 + \frac{\gamma}{\gamma - 1} \frac{p}{\rho} - \Omega_i R \mathbf{u} \cdot \hat{\phi}, \quad (14)$$

$$p = \sigma_i \rho^\gamma, \quad (15)$$

$$0 = \left[\frac{1}{2} \mathbf{B}^2 + p \right]. \quad (16)$$

In contrast to the zero-flow limit, pressure is not constant in each plasma region, but instead there are non-zero pressure gradients. This model was discussed in detail in our earlier work.¹⁸

2. Conservation of entropy

Instead of assuming the adiabatic equation of state, an alternative is to conserve the plasma entropy

$$S_i = \int_{\mathcal{R}_i} \frac{1}{\gamma - 1} \rho \ln \left(\frac{p}{\rho^\gamma} \right) d^3 \tau. \quad (17)$$

In this case, the energy functional Eq. (11) gains the additional term $-\sum_i T_i (S_i - S_i^0)$, where T_i is a Lagrange multiplier that will be identified as the plasma temperature.

The minimum energy states of this model satisfy

$$\nabla \times \mathbf{B} = \mu_i \mathbf{B} + \lambda_i \nabla \times \mathbf{u}, \quad (18)$$

$$\rho \mathbf{u} = \lambda_i \mathbf{B} + \rho \Omega_i R \hat{\phi}, \quad (19)$$

$$\nu_i = \frac{1}{2} \mathbf{u}^2 - \frac{T_i}{\gamma - 1} \left[\ln \left(\frac{p}{\rho^\gamma} \right) - \gamma \right] - \Omega_i R \mathbf{u} \cdot \hat{\phi}, \quad (20)$$

$$p = \rho T_i, \quad (21)$$

$$0 = \left[\frac{1}{2} \mathbf{B}^2 + p \right], \quad (22)$$

where from Eq. (21) we can identify the Lagrange multiplier T_i as the plasma temperature in each region (in units where the Boltzmann constant $k_B = 1$). The model given by Eqs. (18)–(22) is the isotropic limit of the anisotropic MRxMHD model presented in Sec. III. A derivation of that model is given in Appendix A.

In this model, the plasma has constant temperature T_i in each region. Note that in deriving Eq. (21), we have not assumed that the plasma obeys an isothermal equation of state during relaxation, as the temperature T_i is not known *a priori*. Instead, the final equilibrium temperatures in each region are determined by the conservation of plasma entropy in each region, and may change from their initial values.

In the zero-flow limit, the conservation of entropy approach is equivalent to assuming the adiabatic equation of state. In this limit, the two are related by $\sigma_i = \exp[(\gamma - 1)S_i^0/M_i^0]$. Thus in the zero-flow limit, both MRxMHD flow models reduce to the zero-flow model presented in Sec. II A.

C. Including the effects of pressure anisotropy

We present here an extension to MRxMHD to include the effects of pressure anisotropy. This model is an extension to our previous work that included the effects of bulk plasma flow,¹⁸ and includes ideas from the work of Sun and Finn.¹ In our model, each plasma region is assumed to have

undergone a generalized type of Taylor relaxation which minimizes the plasma energy

$$E = \sum_i E_i = \sum_i \int_{\mathcal{R}_i} \left(\frac{1}{2} \rho \mathbf{u}^2 + \frac{1}{2} \mathbf{B}^2 + \frac{1}{2} p_{\parallel} + p_{\perp} \right) d^3 \tau \quad (23)$$

subject to constraints of the plasma mass M_i (Eq. (2)), magnetic helicity K_i (Eq. (3)), flow helicity C_i (Eq. (9)), angular momentum L_i (Eq. (10)), and the additional quantities

$$S_i = \int_{\mathcal{R}_i} \frac{1}{2} \rho \ln \left(\frac{p_{\parallel} p_{\perp}^2}{\rho^5} \right) d^3 \tau, \quad (24)$$

$$G_i[F] = \int_{\mathcal{R}_i} \rho F \left(\frac{p_{\perp}}{\rho B} \right) d^3 \tau, \quad (25)$$

where S_i is the anisotropic plasma entropy, and $G_i[F]$ is a conserved quantity related to the magnetic moment of the plasma gyro-motion, which is written in terms of the unspecified function $F(p_{\perp}/\rho B)$. Additionally, p_{\parallel} and p_{\perp} are the parallel and perpendicular pressures, and $B = |\mathbf{B}|$ is the magnitude of the magnetic field. The plasma quantities constrained by this model are all conserved by the double-adiabatic anisotropic ideal MHD model (the Chew-Goldberger-Low model²²) and are assumed to be robust in the presence of small amounts of resistivity and viscosity. The anisotropic entropy (Eq. (24)) reduces to the isotropic entropy (Eq. (17)) in the limit $p_{\parallel} = p_{\perp}$ with $\gamma = 5/3$.

The constraints S_i and G_i are a generalization of the parallel and perpendicular entropies defined by Sun and Finn¹

$$S_{\parallel} = \int \rho \ln \left(\frac{p_{\parallel} B^2}{\rho^3} \right) d^3 \tau, \quad (26)$$

$$S_{\perp} = \int \rho \ln \left(\frac{p_{\perp}}{\rho B} \right) d^3 \tau, \quad (27)$$

where $S_i = \frac{1}{2} S_{\parallel} + S_{\perp}$ and $G_i = S_{\perp}$ with the function $F(x)$ in Eq. (25) given by the choice $F(x) = \ln(x)$. Hence, our choice of constraints S_i and G_i include those considered by Sun and Finn,¹ but are more general as the function $F(x)$ is unspecified. This unspecified function can be thought of as an anisotropic equation of state, and in Sec. III A is shown to be related to the anisotropic plasma enthalpy. Another valid choice for $F(x)$ is $F(x) = x$, which corresponds to constraining the quantity $\int (p_{\perp}/B) d^3 \tau$. We show in Sec. III A that this choice of $F(x)$ is equivalent to the two-temperature guiding-centre plasma equation of state in anisotropic ideal MHD.²³

The choice to constrain the quantity G_i is motivated by the magnetic moment adiabatic invariant $\tilde{\mu}$, in which the CGL anisotropic MHD model,²² is assumed to be constant along magnetic field lines

$$\frac{d}{dt} \tilde{\mu} = \frac{d}{dt} \left(\frac{p_{\perp}}{\rho B} \right) = 0. \quad (28)$$

This equation of motion corresponds to the infinity of constraints

$$G[F] = \int \rho F \left(\frac{p_{\perp}}{\rho B} \right) d^3 \tau \quad (29)$$

for all functions $F(x)$. The model presented in this work selects one element of this class of invariants as the most conserved of this class. Choosing the function $F(x)$ specifies this choice and is effectively an anisotropic equation of state.

Minimum energy states of the MRxMHD model with anisotropy and flow are stationary points of the energy functional

$$W = \sum_i \left[E_i - \nu_i (M_i - M_i^0) - \frac{1}{2} \mu_i (K_i - K_i^0) - \lambda_i (C_i - C_i^0) - \Omega_i (L_i - L_i^0) - T_i (S_i - S_i^0) - \eta_i (G_i - G_i^0) \right], \quad (30)$$

where η_i is a Lagrange multiplier enforcing the constraint on the quantity G_i .

Setting the first variation of Eq. (30) to zero gives the plasma region conditions

$$\nabla \times \mathbf{B} = \mu_i \mathbf{B} + \lambda_i \nabla \times \mathbf{u} + \nabla \times \left[\left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \mathbf{B} \right], \quad (31)$$

$$\rho \mathbf{u} = \lambda_i \mathbf{B} + \rho \Omega_i R \hat{\phi}, \quad (32)$$

$$\nu_i = \frac{1}{2} \mathbf{u}^2 - \frac{1}{2} T_i \left[\ln \left(\frac{p_{\parallel} p_{\perp}^2}{\rho^5} \right) - 5 \right] - \eta_i F \left(\frac{p_{\perp}}{\rho B} \right) - \frac{p_{\parallel} - p_{\perp}}{\rho} - \Omega_i R \mathbf{u} \cdot \hat{\phi}, \quad (33)$$

$$p_{\parallel} = \rho T_i, \quad (34)$$

$$p_{\perp} = \rho T_i + \eta_i \frac{p_{\perp}}{B} F' \left(\frac{p_{\perp}}{\rho B} \right) \quad (35)$$

together with the interface force-balance condition

$$\left[\left[\frac{1}{2} \mathbf{B}^2 + p_{\perp} \right] \right] = 0. \quad (36)$$

A derivation of these equations is given in Appendix A.

Taking the isotropic limit ($\eta = 0$) gives MRxMHD with flow with conserved entropy (see Sec. II B 2) with $\gamma = 5/3$.

In Appendix B, we show that the MRxMHD minimum energy states described by Eqs. (31)–(35) satisfy

$$\rho (\mathbf{u} \cdot \nabla) \mathbf{u} = -\nabla \cdot \vec{P} + \mathbf{J} \times \mathbf{B} - \rho \Omega_i R \hat{\phi} \times (\nabla \times \mathbf{u}) + \rho \Omega_i \nabla (R \mathbf{u} \cdot \hat{\phi}), \quad (37)$$

where \vec{P} is the pressure tensor, which is given by

$$\vec{P} = p_{\perp} \vec{I} + (p_{\parallel} - p_{\perp}) \mathbf{B} \mathbf{B} / B^2, \quad (38)$$

with \vec{I} the identity tensor. The last two terms on the right-hand side of Eq. (37) are perhaps unexpected, and are

discussed in further detail below. In the limit that the plasma minimum energy state is axisymmetric, these two terms are zero,¹⁸ and we recover the expected anisotropic ideal MHD equilibrium equation

$$\rho(\mathbf{u} \cdot \nabla)\mathbf{u} = -\nabla \cdot \vec{P} + \mathbf{J} \times \mathbf{B}. \quad (39)$$

We discussed the effect of the last two terms of Eq. (37) in the context of isotropic MRxMHD with flow in Dennis *et al.*,¹⁸ indeed, Eq. (37) is identical to Eq. (16) of Dennis *et al.*¹⁸ with $\nabla \cdot \vec{P}$ replacing ∇p . For stellarators or other plasmas with a fixed non-axisymmetric outer boundary, these terms do not appear because (in the absence of any proof to the contrary) it must be assumed that even a smooth rigid outer boundary may exert a torque on a flowing plasma. In Dennis *et al.*,¹⁸ we showed that a contradiction would arise if toroidal angular momentum was assumed to be conserved. Thus toroidal angular momentum cannot be assumed to be conserved, and therefore the angular momentum terms must be dropped from Eq. (30) (i.e., the Ω_i are zero). The last two terms of Eq. (37) are only non-zero for non-axisymmetric minimum energy states with a (fixed) axisymmetric outer boundary. In this case, Eq. (37) is equivalent to force-balance in a reference frame rotating about the Z axis with angular frequency Ω_i . These non-axisymmetric equilibria will be time-dependent in the laboratory frame, but will be time-independent in a reference frame rotating with angular frequency Ω_i about the Z axis. This feature was discussed in detail in our earlier work on MRxMHD with flow.¹⁸

1. Choices for the function $F(x)$

If the choice $F(x) = \ln(x)$ is made as in Sun and Finn,¹ then the parallel and perpendicular temperatures are constant in each plasma region

$$p_{\parallel} = \rho T_i, \quad (40)$$

$$p_{\perp} = \rho(\eta_i + T_i). \quad (41)$$

The Bernoulli equation (Eq. (33)) becomes

$$\begin{aligned} \nu_i = \frac{1}{2}\mathbf{u}^2 - \frac{1}{2}T_i \left[\ln \left(\frac{T_i(T_i + \eta_i)^2}{\rho^2} \right) - 5 \right] \\ - \eta_i \left[\ln \left(\frac{T_i + \eta_i}{B} \right) - 1 \right] - \Omega_i R \mathbf{u} \cdot \hat{\phi}. \end{aligned} \quad (42)$$

If instead the choice $F(x) = x$ is made, then the parallel temperature is constant in each plasma region, but the perpendicular temperature depends on the magnitude of the magnetic field B

$$p_{\parallel} = \rho T_i, \quad (43)$$

$$p_{\perp} = \rho T_i \frac{B}{B - \eta_i}. \quad (44)$$

The Bernoulli equation (Eq. (33)) becomes

$$\begin{aligned} \nu_i = \frac{1}{2}\mathbf{u}^2 - \frac{1}{2}T_i \left[\ln \left(\frac{T_i^3}{\rho^2(1 - \eta_i/B)^2} \right) - 5 \right] \\ - \Omega_i R \mathbf{u} \cdot \hat{\phi}. \end{aligned} \quad (45)$$

The pressure equations given by Eqs. (43)–(44) are identical to those of the guiding-centre plasma two-temperature closure relations (see Eq. (34) of Iacono *et al.*²³). It is shown in Sec. III that the choice $F(x) = x$ corresponds identically to this model in the continuously nested flux surface limit.

2. Summary

We have presented a multi-region relaxation model for plasmas which includes both anisotropy and flow. We validate our model in Sec. III by proving that it approaches anisotropic ideal MHD with flow in the limit as the number of plasma volumes N becomes large, and this is independent of the choice of the function $F(x)$. We have previously proven that MRxMHD with flow approaches ideal MHD with flow.¹⁸

III. THE CONTINUOUSLY NESTED FLUX-SURFACE LIMIT

In this section, we take the continuously nested flux surface limit ($N \rightarrow \infty$) of anisotropic MRxMHD and prove that it reduces to anisotropic ideal MHD.

Taking the limit of infinitesimally small plasma regions of the energy functional Eq. (30) gives

$$\begin{aligned} W = \int \left(\frac{1}{2}\rho\mathbf{u}^2 + \frac{1}{2}\mathbf{B}^2 + \frac{1}{2}p_{\parallel} + p_{\perp} \right) d^3\tau \\ - \int \nu(s)(dM - dM^0) - \int \frac{1}{2}\mu(s)(dK - dK^0) \\ - \int \lambda(s)(dC - dC^0) - \int \Omega(s)(dL - dL^0) \\ - \int T(s)(dS - dS^0) - \int \eta(s)(dG - dG^0), \end{aligned} \quad (46)$$

where s is an arbitrary flux-surface label; dM , dK , dC , dL , dS and dG are, respectively, infinitesimal amounts of plasma mass, magnetic helicity, flow helicity, toroidal angular momentum, plasma entropy, and the magnetic dipole constraint G between infinitesimally separated flux surfaces; and dM^0 , dK^0 , dC^0 , dL^0 , dS^0 , and dG^0 are the corresponding constraints.

In the finite-volume limit, the magnetic flux constraints are enforced by restricting the class of perturbations of the vector potential $\delta\mathbf{A}$ (see Appendix A), and these constraints are therefore not included in the energy functional given by Eq. (46). In the limit of continuously nested flux surfaces, we use the same approach we used in Dennis *et al.*¹⁸ and introduce a vector of Lagrange multipliers $\mathbf{Q} = Q_s(s, \theta, \zeta)\nabla s + Q_{\theta}(s)\nabla\theta + Q_{\zeta}(s)\nabla\zeta$ to enforce the radial, poloidal, and toroidal magnetic flux constraints in an (s, θ, ζ) coordinate system with θ an arbitrary poloidal angle coordinate and ζ an arbitrary toroidal angle coordinate. As detailed in Sec. III A of Dennis *et al.*,¹⁸ enforcing the magnetic flux constraints

requires adding the following terms to the right-hand side of the energy functional Eq. (46)

$$W|_{\text{flux constraints}} = - \int (\mathbf{Q} \cdot \mathbf{B}) d^3\tau + 2\pi \int \left[Q_\theta(s) \frac{d\psi_p^0(s)}{ds} + Q_\zeta(s) \frac{d\psi_t^0(s)}{ds} \right] ds, \quad (47)$$

where $\psi_p(s)$ and $\psi_t(s)$ are, respectively, the poloidal and toroidal magnetic fluxes enclosed by the flux surface with label s .

In Dennis *et al.*,¹⁸ we showed that the magnetic helicity constraint is trivially satisfied in the limit of continuously nested flux surfaces with $dK = dK^0$ following from conservation of the magnetic fluxes within every flux surface. Therefore the magnetic helicity term $\int \frac{1}{2} \mu(s) (dK - dK^0) ds$ in Eq. (46) is zero.

With these simplifications, we obtain the energy functional

$$W = \int \left[\frac{1}{2} \rho \mathbf{u}^2 + \frac{1}{2} \mathbf{B}^2 + \frac{1}{2} p_{\parallel} + p_{\perp} - \mathbf{Q} \cdot \mathbf{B} - \nu(s) \rho - \lambda(s) \mathbf{B} \cdot \mathbf{u} - \rho \Omega(s) R \mathbf{u} \cdot \hat{\phi} - \frac{1}{2} T(s) \rho \ln \left(\frac{p_{\parallel} p_{\perp}^2}{\rho^5} \right) - \eta(s) \rho F \left(\frac{p_{\perp}}{\rho B} \right) \right] d^3\tau + \int \left[2\pi Q_\theta(s) \frac{d\psi_p^0(s)}{ds} + 2\pi Q_\zeta(s) \frac{d\psi_t^0(s)}{ds} + \nu(s) \frac{dM^0(s)}{ds} + \lambda(s) \frac{dC^0(s)}{ds} + \Omega(s) \frac{dL^0(s)}{ds} + T(s) \frac{dS^0(s)}{ds} + \eta(s) \frac{dG^0(s)}{ds} \right] ds. \quad (48)$$

Requiring zero variations of W with respect to the Lagrange multipliers enforces the corresponding constraints. The interesting variations are those with respect to p_{\parallel} , p_{\perp} , ρ , \mathbf{u} , \mathbf{B} , and the position of the flux surfaces \mathbf{x} .

Setting the variation of W with respect to p_{\parallel} , p_{\perp} , ρ , \mathbf{u} , and \mathbf{B} to zero yield, respectively

$$p_{\parallel} = \rho T(s), \quad (49)$$

$$p_{\perp} = \rho T(s) + \eta(s) \frac{p_{\perp}}{B} F' \left(\frac{p_{\perp}}{\rho B} \right), \quad (50)$$

$$\nu(s) = \frac{1}{2} \mathbf{u}^2 - \frac{1}{2} T(s) \left[\ln \left(\frac{p_{\parallel} p_{\perp}^2}{\rho^5} \right) - 5 \right] - \eta(s) F \left(\frac{p_{\perp}}{\rho B} \right) - \frac{p_{\parallel} - p_{\perp}}{\rho} - \Omega(s) R \mathbf{u} \cdot \hat{\phi}, \quad (51)$$

$$\rho \mathbf{u} = \lambda(s) \mathbf{B} + \rho \Omega(s) R \hat{\phi}, \quad (52)$$

$$\mathbf{Q} = \mathbf{B} - \lambda(s) \mathbf{u} - \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \mathbf{B}. \quad (53)$$

Using a very similar process to our earlier work,¹⁸ the variation of W with respect to $\delta \mathbf{x}$ can be simplified to obtain

$$\delta W|_{\delta \mathbf{x}} = \int \delta \mathbf{x} \cdot [\rho (\mathbf{u} \cdot \nabla) \mathbf{u} - \mathbf{J} \times \mathbf{B} + \nabla \cdot \vec{P} + \rho \Omega R \hat{\phi} \times (\nabla \times \mathbf{u}) - \rho \Omega \nabla (R \mathbf{u} \cdot \hat{\phi})], \quad (54)$$

where we have used

$$\nabla \cdot \vec{P} = \nabla p_{\perp} + \mathbf{B} (\mathbf{B} \cdot \nabla) \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) + \frac{p_{\parallel} - p_{\perp}}{B^2} (\mathbf{B} \cdot \nabla) \mathbf{B}, \quad (55)$$

which follows from the definition of the pressure tensor \vec{P} given by Eq. (38).

Setting the variation $\delta W|_{\delta \mathbf{x}}$ to zero gives

$$\rho (\mathbf{u} \cdot \nabla) \mathbf{u} = - \nabla \cdot \vec{P} + \mathbf{J} \times \mathbf{B} - \rho \Omega(s) R \hat{\phi} \times (\nabla \times \mathbf{u}) + \rho \Omega(s) \nabla (R \mathbf{u} \cdot \hat{\phi}), \quad (56)$$

which is identical to Eq. (37) with the replacement $\Omega_i \rightarrow \Omega(s)$, and is an equation for force-balance in a reference frame rotating with angular velocity $\Omega(s)$ about the \mathbf{Z} axis.

A. The relationship between $F(\mathbf{x})$ and plasma enthalpy

The anisotropic ideal MHD Bernoulli equation is usually written in terms of an unspecified plasma enthalpy²⁴ $H(\rho, B, s)$

$$\nu(s) = \frac{1}{2} \mathbf{u}^2 - \Omega(s) R \mathbf{u} \cdot \hat{\phi} + H(\rho, B, s). \quad (57)$$

To satisfy conservation of energy, the enthalpy must satisfy the integrability conditions²³

$$\left(\frac{\partial H}{\partial \rho} \right)_{B,s} = \frac{1}{\rho} \left(\frac{\partial p_{\parallel}}{\partial \rho} \right)_{B,s}, \quad (58)$$

$$\left(\frac{\partial H}{\partial B} \right)_{\rho,s} = \frac{1}{\rho} \left[\left(\frac{\partial p_{\parallel}}{\partial B} \right)_{\rho,s} - \frac{p_{\parallel} - p_{\perp}}{B} \right]. \quad (59)$$

By comparison with the Bernoulli equation we have derived, Eq. (51), we can identify the plasma enthalpy to be

$$H(\rho, B, s) = -\frac{1}{2} T(s) \left[\ln \left(\frac{p_{\parallel} p_{\perp}^2}{\rho^5} \right) - 5 \right] - \eta(s) F \left(\frac{p_{\perp}}{\rho B} \right) - \frac{p_{\parallel} - p_{\perp}}{\rho}, \quad (60)$$

which can be shown to satisfy the integrability conditions Eqs. (58) and (59) for any choice of $F(x)$.

If the function F is chosen to be $F(x) = x$, then similar expressions to what were obtained in the finite plasma region limit, we obtain expressions for the plasma pressures

$$p_{\parallel} = \rho T(s), \quad (61)$$

$$p_{\perp} = \rho T(s) \frac{B}{B - \eta(s)}, \quad (62)$$

which are identical to the equations of state for the two-temperature guiding-centre plasma model (see Iacono *et al.*²³).

B. Summary

We have now proven that as the number of plasma regions N becomes large in the anisotropic MRxMHD with flow model that the model reduces to anisotropic ideal MHD with flow. The minimum energy state may not be time-independent in the laboratory reference frame, but will be time-independent in a rotating reference frame depending on the symmetry assumptions made in the model (see Dennis *et al.*¹⁸ for details).

The energy functional given by Eq. (48) also represents the first variational principle for anisotropic plasma equilibria with general flow fields. This variational principle can be considered to be a generalization of that for isotropic plasma equilibria with flow described by Hameiri.¹⁴

In Sec. IV, we provide a simple example calculation using our anisotropic MRxMHD model.

IV. EXAMPLE APPLICATION

In this section, we apply our anisotropic MRxMHD model to an RFP-like plasma in the zero-flow limit. We have previously presented a calculation with finite flow in the isotropic limit in earlier work.¹⁸ Our example calculation is motivated by the experimental results of Sasaki *et al.*,²⁵ who observed ion temperature anisotropy in the EXTRAP-T2 reversed-field pinch. In their work, Sasaki *et al.* measured the parallel ion temperature to be 1–3 times larger than the perpendicular temperature. Anisotropic plasma pressures have also been observed on MST during reconnection events,²⁶ however on that experiment, the perpendicular temperature was observed to be greater. In this example, we focus on the results of the EXTRAP-T2 experiment.

We model EXTRAP-T2 experiment of Sasaki *et al.* with single-volume anisotropic MRxMHD with zero plasma flow. Additionally, we choose $F(x) = \ln(x)$ in Eq. (25) as this yields a constant ratio of parallel to perpendicular temperature, which accords with the analysis of Sasaki *et al.* In this limit, the anisotropic MRxMHD equations (Eqs. (31)–(35)) in SI units are

$$\nabla \times \mathbf{B} = \mu \mathbf{B} - k_B \eta \nabla \times \left(\frac{\mu_0 \rho}{B^2} \mathbf{B} \right), \quad (63)$$

$$\rho = \rho_0 \left(\frac{B}{B_0} \right)^{-\eta/T}, \quad (64)$$

$$p_{\parallel} = \rho k_B T, \quad (65)$$

$$p_{\perp} = \rho k_B (T + \eta), \quad (66)$$

where ρ_0 is a constant reference density, B_0 is a constant reference magnetic field, and k_B is Boltzmann's constant.

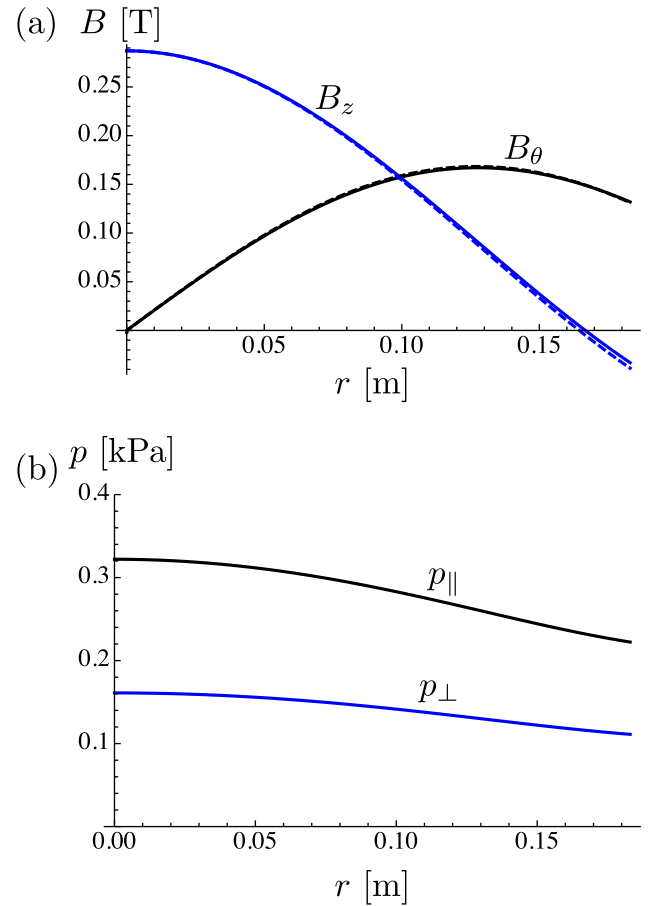


FIG. 2. Example anisotropic MRxMHD solution for an RFP in cylindrical geometry with a single plasma volume. Panels (a) and (b), respectively, show the magnetic field components and plasma pressure versus radial position. The dashed lines in panel (a) indicate the magnetic field profile expected if the pressure was assumed to be isotropic ($\eta = 0$).

Figure 2 illustrates the results of this model. The equilibrium is described by $\mu = 14.4 \text{ m}^{-1}$, $T = 250 \text{ eV}$, $\eta = -170 \text{ eV}$, $\rho_0 = 8.9 \times 10^{19} \text{ m}^{-3}$, with $B_0 = 1 \text{ T}$. These values have been chosen to ensure that the model agrees with the average experimental parameters observed during $t \approx 7\text{--}9 \text{ ms}$ in Figure 2 of Sasaki *et al.*,²⁵ namely major radius $R = 1.24 \text{ m}$, minor radius $a = 0.183 \text{ m}$, plasma current $I_p \approx 120 \text{ kA}$, reversal parameter $F \approx -0.4$, on-axis electron number density $\rho_e \approx 1.9 \times 10^{19} \text{ m}^{-3}$, parallel temperature $T_{\parallel} \approx 250 \text{ eV}$, perpendicular temperature $T_{\perp} \approx 80 \text{ eV}$.

A significant difference from the isotropic zero-flow limit presented in Sec. II A is that although the parallel and perpendicular temperatures are constant in each region, the pressures are not due to the variation of the plasma density with magnetic field strength B given by Eq. (64). In the isotropic limit, the plasma density becomes independent of the magnetic field strength, and the pressure becomes constant in each plasma region, in agreement with Eq. (6).

V. CONCLUSION

We have formulated an energy principle for equilibria that comprise multiple Taylor-relaxed plasma regions, including the effects of plasma anisotropy and flow. This model is an extension of our earlier work that considered the

isotropic finite-flow limit,¹⁸ and the work of Sun and Finn¹ who considered a special case of the single relaxed-region anisotropic zero-flow limit. We have demonstrated that our model reduces to anisotropic ideal MHD with flow in the limit of an infinite number of plasma regions. This limit demonstrates the validity of our anisotropic MRxMHD model, and is, to our knowledge, the first variational principle for anisotropic plasma equilibria with general flow fields. The numerical solution to the anisotropic MRxMHD model with flow presented in this work will be the subject of future work as an extension to the Stepped Pressure Equilibrium Code (SPEC).²⁷ Implementation of the anisotropic MRxMHD model into SPEC will enable detailed comparisons between the predictions of our model in the case of fully 3D plasmas with multiple relaxed-regions and high-performance anisotropic tokamak discharges.

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APPENDIX A: DERIVATION OF THE MRxMHD EQUATIONS

In this appendix, we derive the Euler-Lagrange equations for the plasma, Eqs. (31)–(36). The anisotropic plasma equations for a single volume have been obtained previously by Sun and Finn¹ in the zero-flow limit and taking the function $F(x) = \ln(x)$ in the magnetic dipole constraint G (see Eq. (25)). Here, we extend that work by considering multiple nested volumes, arbitrary functions $F(x)$, and including the effects of plasma flow. Our derivation is a generalization of our earlier work¹⁸ to include anisotropy.

Equilibria of the anisotropic MRxMHD model are stationary points of the energy functional Eq. (30)

$$W = \sum_i \left[E_i - \nu_i (M_i - M_i^0) - \frac{1}{2} \mu_i (K_i - K_i^0) - \lambda_i (C_i - C_i^0) - \Omega_i (L_i - L_i^0) - T_i (S_i - S_i^0) - \eta_i (G_i - G_i^0) \right], \quad (\text{A1})$$

where ν_i , μ_i , λ_i , Ω_i , T_i , and η_i are Lagrange multipliers and E_i , M_i , K_i , C_i , L_i , S_i , and G_i are defined in Sec. II.

Instead of introducing Lagrange multipliers to enforce the toroidal and poloidal flux constraints as in Sec. III, we use the approach of Spies *et al.*²⁸ who showed that the flux constraints are equivalent to the following relationship at the interfaces:

$$\mathbf{n} \times \delta \mathbf{A} = -(\mathbf{n} \cdot \delta \mathbf{x}) \mathbf{B}, \quad (\text{A2})$$

where \mathbf{n} is a unit normal vector perpendicular to the interface boundary, $\delta \mathbf{A}$ is the variation of the vector potential, and $\delta \mathbf{x}$ is the perturbation to the interface positions.

Setting the variations of W with respect to \mathbf{u} , ρ , p_{\parallel} , and p_{\perp} to zero yield, respectively

$$\rho \mathbf{u} = \lambda_i \mathbf{B} + \rho \Omega_i R \hat{\phi}, \quad (\text{A3})$$

$$\nu_i = \frac{1}{2} \mathbf{u}^2 - \frac{1}{2} T_i \left[\ln \left(\frac{p_{\parallel} p_{\perp}^2}{\rho^5} \right) - 5 \right] - \eta_i \left[F \left(\frac{p_{\perp}}{\rho B} \right) - \frac{p_{\perp}}{\rho B} F' \left(\frac{p_{\perp}}{\rho B} \right) \right] - \Omega_i R \mathbf{u} \cdot \hat{\phi}, \quad (\text{A4})$$

$$p_{\parallel} = \rho T_i, \quad (\text{A5})$$

$$p_{\perp} = \rho T_i + \eta_i \frac{p_{\perp}}{B} F' \left(\frac{p_{\perp}}{\rho B} \right), \quad (\text{A6})$$

which are equivalent to Eqs. (32)–(35).

The variation of W with respect to \mathbf{A} is

$$\begin{aligned} \delta W|_{\delta \mathbf{A}} = & \sum_i \int_{\mathcal{R}_i} \delta \mathbf{A} \cdot \left\{ \nabla \times \mathbf{B} - \lambda_i \nabla \times \mathbf{u} - \mu_i \mathbf{B} \right. \\ & \left. + \eta_i \nabla \times \left[\frac{p_{\perp}}{B^3} F' \left(\frac{p_{\perp}}{\rho B} \right) \right] \right\} \\ & - \sum_i \oint_{\partial \mathcal{R}_i} (\mathbf{n} \cdot \delta \mathbf{x}) \left[\mathbf{B}^2 - \frac{1}{2} \mu_i \mathbf{A} \cdot \mathbf{B} - \lambda_i \mathbf{u} \cdot \mathbf{B} \right. \\ & \left. + \eta_i \frac{p_{\perp}}{B} F' \left(\frac{p_{\perp}}{\rho B} \right) \right], \quad (\text{A7}) \end{aligned}$$

where $\partial \mathcal{R}_i = \mathcal{I}_{i-1} \cup \mathcal{I}_i$ is the boundary of the plasma volume \mathcal{R}_i , and \mathcal{I}_i is the plasma interface separating plasma volumes \mathcal{R}_{i-1} and \mathcal{R}_i (see Figure 1). The magnetic flux boundary condition, Eq. (A2), has also been used in Eq. (A7) to write the variation of the vector potential $\delta \mathbf{A}$ on the interfaces in terms of the variation to the plasma interfaces $\delta \mathbf{x}$.

Requiring $\delta W|_{\delta \mathbf{A}}$ to be zero for all choices of $\delta \mathbf{A}$ yields

$$\nabla \times \mathbf{B} = \mu_i \mathbf{B} + \lambda_i \nabla \times \mathbf{u} - \eta_i \nabla \times \left[\frac{p_{\perp}}{B^3} F' \left(\frac{p_{\perp}}{\rho B} \right) \right], \quad (\text{A8})$$

which is identical to Eq. (31) upon using the identity

$$\frac{p_{\parallel} - p_{\perp}}{B^2} = -\eta_i \frac{p_{\perp}}{B^3} F' \left(\frac{p_{\perp}}{\rho B} \right), \quad (\text{A9})$$

which follows from Eqs. (A5) and (A6).

The interface condition can now be obtained by considering the variation of W with respect to the interface positions

$$\begin{aligned} \delta W|_{\delta \mathbf{x}} = & \sum_i \oint_{\partial \mathcal{R}_i} (\mathbf{n} \cdot \delta \mathbf{x}) \left[\frac{1}{2} \rho \mathbf{u}^2 + \frac{1}{2} \mathbf{B}^2 + \frac{1}{2} p_{\parallel} + p_{\perp} \right. \\ & - \nu_i \rho - \lambda_i \mathbf{B} \cdot \mathbf{u} - \rho \Omega_i R \mathbf{u} \cdot \hat{\phi} - \frac{1}{2} \mu_i \mathbf{A} \cdot \mathbf{B} \\ & - \left[-\frac{1}{2} T_i \rho \ln \left(\frac{p_{\parallel} p_{\perp}^2}{\rho^5} \right) - \eta_i \rho F \left(\frac{p_{\perp}}{\rho B} \right) \right] \\ & - \sum_i \oint_{\partial \mathcal{R}_i} (\mathbf{n} \cdot \delta \mathbf{x}) \left[\mathbf{B}^2 - \frac{1}{2} \mu_i \mathbf{A} \cdot \mathbf{B} - \lambda_i \mathbf{u} \cdot \mathbf{B} \right. \\ & \left. + \eta_i \frac{p_{\perp}}{B} F' \left(\frac{p_{\perp}}{\rho B} \right) \right], \quad (\text{A10}) \end{aligned}$$

where the remaining term of Eq. (A7) has been included.

Equation (A10) simplifies to

$$\delta W|_{\delta \mathbf{x}} = \sum_i \oint_{\mathcal{I}_i} (\mathbf{n} \cdot \delta \mathbf{x}) \left[\left[\frac{1}{2} \mathbf{B}^2 + p_{\perp} \right] \right], \quad (\text{A11})$$

where $[[x]] = x_{i+1} - x_i$ is the jump in x across the plasma interface \mathcal{I}_i . Requiring this variation to be zero gives the interface condition Eq. (36)

$$\left[\left[\frac{1}{2} \mathbf{B}^2 + p_{\perp} \right] \right] = 0. \quad (\text{A12})$$

APPENDIX B: PROOF THAT MRxMHD SOLUTIONS SATISFY ANISOTROPIC FORCE-BALANCE

In this appendix, we show that the minimum energy MRxMHD states described by the Euler-Lagrange equations, Eqs. (31)–(36), satisfy the anisotropic rotating-frame force-balance condition Eq. (37).

The magnetic field in each plasma region obeys Eq. (31), which is

$$\nabla \times \mathbf{B} = \mu_i \mathbf{B} + \lambda_i \nabla \times \mathbf{u} + \nabla \times \left[\left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \mathbf{B} \right]. \quad (\text{B1})$$

Taking the cross-product of this with \mathbf{B} yields

$$\mathbf{J} \times \mathbf{B} = -\lambda_i \mathbf{B} \times (\nabla \times \mathbf{u}) - \mathbf{B} \left\{ \nabla \times \left[\left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \mathbf{B} \right] \right\}. \quad (\text{B2})$$

The first term on the right-hand side of Eq. (B2) can be simplified using Eq. (32) to give

$$-\lambda_i \mathbf{B} \times (\nabla \times \mathbf{u}) = \rho \Omega_i R \hat{\phi} \times (\nabla \times \mathbf{u}) - \frac{1}{2} \rho \nabla u^2 + \rho (\mathbf{u} \cdot \nabla) \mathbf{u}. \quad (\text{B3})$$

Substitution back into Eq. (B2) gives

$$\rho (\mathbf{u} \cdot \nabla) \mathbf{u} = \mathbf{J} \times \mathbf{B} - \rho \Omega_i R \hat{\phi} \times (\nabla \times \mathbf{u}) + \frac{1}{2} \rho \nabla u^2 + \mathbf{B} \times \left\{ \nabla \times \left[\left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \mathbf{B} \right] \right\}. \quad (\text{B4})$$

Next we need to use the Bernoulli equation, Eq. (33), to write the $\rho \nabla u^2$ term in Eq. (B4) as an expression involving the divergence of the pressure tensor. Using Eq. (34), the Bernoulli equation can be written as

$$\begin{aligned} \nu_i &= \frac{1}{2} u^2 - \frac{1}{2} T_i \left[\ln \left(\frac{T_i p_{\perp}^2}{\rho^4} - 5 \right) \right] \\ &\quad - \eta_i F \left(\frac{p_{\perp}}{\rho B} \right) - T_i + \frac{p_{\perp}}{\rho} - \Omega_i R \mathbf{u} \cdot \hat{\phi}. \end{aligned} \quad (\text{B5})$$

We take the gradient of the Bernoulli equation to obtain an expression involving $\rho \nabla u^2$

$$\begin{aligned} 0 &= \frac{1}{2} \nabla u^2 - \frac{1}{2} T_i \left(2 \frac{\nabla p_{\perp}}{p_{\perp}} - 4 \frac{\nabla \rho}{\rho} \right) \\ &\quad - \eta_i F' \left(\frac{p_{\perp}}{\rho B} \right) \left(\frac{p_{\perp}}{\rho B} \right) \left(\frac{\nabla p_{\perp}}{p_{\perp}} - \frac{\nabla \rho}{\rho} - \frac{\nabla B}{B} \right) \\ &\quad + \frac{\nabla p_{\perp}}{\rho} - p_{\perp} \frac{\nabla \rho}{\rho^2} - \Omega_i \nabla (R \mathbf{u} \cdot \hat{\phi}). \end{aligned} \quad (\text{B6})$$

Using Eq. (A9) to rewrite F' in terms of physical quantities gives

$$\begin{aligned} \frac{1}{2} \nabla u^2 &= T_i \left(\frac{\nabla p_{\perp}}{p_{\perp}} - 2 \frac{\nabla \rho}{\rho} \right) + \frac{p_{\perp}}{\rho^2} \nabla \rho - \frac{\nabla p_{\perp}}{\rho} \\ &\quad - \frac{p_{\parallel} - p_{\perp}}{\rho} \left(\frac{\nabla p_{\perp}}{p_{\perp}} - \frac{\nabla \rho}{\rho} - \frac{\nabla B}{B} \right) \\ &\quad + \Omega_i \nabla (R \mathbf{u} \cdot \hat{\phi}), \end{aligned} \quad (\text{B7})$$

which can be simplified to

$$\frac{1}{2} \rho \nabla u^2 = -\nabla p_{\parallel} + \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \frac{1}{2} \nabla B^2 + \rho \Omega_i \nabla (R \mathbf{u} \cdot \hat{\phi}). \quad (\text{B8})$$

Equation (B8) can now be used to eliminate the $\rho \nabla u^2$ term from Eq. (B4) to give

$$\begin{aligned} \rho (\mathbf{u} \cdot \nabla) \mathbf{u} &= \mathbf{J} \times \mathbf{B} - \rho \Omega_i R \hat{\phi} \times (\nabla \times \mathbf{u}) + \rho \Omega_i \nabla (R \mathbf{u} \cdot \hat{\phi}) \\ &\quad - \nabla p_{\parallel} + \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \frac{1}{2} \nabla B^2 \\ &\quad + \mathbf{B} \times \left\{ \nabla \times \left[\left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \mathbf{B} \right] \right\}. \end{aligned} \quad (\text{B9})$$

This is almost in the desired form of Eq. (37), all that remains to be shown is that the terms on the second and third lines of Eq. (B9) are equal to $-\nabla \cdot \vec{P}$.

The last term of Eq. (B9) can be simplified to give

$$\begin{aligned} \mathbf{B} \times \left\{ \nabla \times \left[\left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \mathbf{B} \right] \right\} &= \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \mathbf{B} \times (\nabla \times \mathbf{B}) + \mathbf{B} \times \left[\nabla \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \times \mathbf{B} \right], \\ &= \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \mathbf{B} \times (\nabla \times \mathbf{B}) + \mathbf{B}^2 \nabla \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \\ &\quad - \mathbf{B} (\mathbf{B} \cdot \nabla) \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right), \\ &= \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) [\mathbf{B} \times (\nabla \times \mathbf{B}) - \nabla B^2] + \nabla (p_{\parallel} - p_{\perp}) \\ &\quad - \mathbf{B} (\mathbf{B} \cdot \nabla) \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right), \\ &= - \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) \left[(\mathbf{B} \cdot \nabla) \mathbf{B} + \frac{1}{2} \nabla B^2 \right] + \nabla (p_{\parallel} - p_{\perp}) \\ &\quad - \mathbf{B} (\mathbf{B} \cdot \nabla) \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right). \end{aligned} \quad (\text{B10})$$

Using this to replace the last term in Eq. (B9) gives

$$\begin{aligned} \rho (\mathbf{u} \cdot \nabla) \mathbf{u} &= \mathbf{J} \times \mathbf{B} - \rho \Omega_i R \hat{\phi} \times (\nabla \times \mathbf{u}) + \rho \Omega_i \nabla (R \mathbf{u} \cdot \hat{\phi}) \\ &\quad - \nabla p_{\perp} - \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right) (\mathbf{B} \cdot \nabla) \mathbf{B} \\ &\quad - \mathbf{B} (\mathbf{B} \cdot \nabla) \left(\frac{p_{\parallel} - p_{\perp}}{B^2} \right), \end{aligned} \quad (\text{B11})$$

where the last three terms are equal to $-\nabla \cdot \vec{P}$ (see Eq. (55)).

We have now shown that the minimum energy MRxMHD states satisfy the anisotropic rotating-frame force-balance condition

$$\rho(\mathbf{u} \cdot \nabla)\mathbf{u} = \mathbf{J} \times \mathbf{B} - \nabla \cdot \vec{P} - \rho\Omega_i R \hat{\phi} \times (\nabla \times \mathbf{u}) + \rho\Omega_i \nabla(R\mathbf{u} \cdot \hat{\phi}). \quad (\text{B12})$$

As shown in Dennis *et al.*,¹⁸ the last two terms of this force-balance condition mean that the plasma may not be time-independent in the laboratory frame, but will be time-independent in a reference frame rotating about the $\hat{\mathbf{Z}}$ axis with angular velocity Ω_i .

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